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## Effect of Pressure on Graphitization of Carbon. I. Heat Treatment of Soft Carbon under 1, 3 and 5 kbar

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Polyvinylchloride coke was heat-treated under the quasi-hydrostatic pressure of 1, 3, and 5 kbar by using a simple piston cylinder type high pressure apparatus. The process of graphitization under pressure was studied kinetically by analyzing the profile of the (002) diffraction line. It was found that the accelerating effect of pressure on the graphitization of carbon became more pronounced at higher pressure. The process of graphitization under 3, and 5 kbar seemed to take place in at least two stages. In the first stage, the profile of the (002) line shifted simply from the position of the original line to  $26.0^\circ$  in  $2\theta$ , which corresponded to a  $c_0$ -spacing of 6.85 Å. In the next stage, a new component, having a  $c_0$ -spacing of about 6.72 Å, appeared in addition to the first component, having a  $c_0$ -spacing of 6.85 Å. Therefore, the profiles of the (002) line became composite. Under 1 kbar, however, no composite profiles were observed and the  $c_0$ -spacing decreased gradually with heat treatment. Approximate values for the activation energy and activation volume for graphitization under 3—5 kbar were estimated to be 80—120 kcal/mol, and  $-7$ — $-9$  cc/mol, respectively.

It has been reported that the graphitizing cokes, such as petroleum coke and polyvinylchloride coke, graphitized very rapidly at around  $1500^\circ\text{C}$  under a pressure of 10 kbar.<sup>1)</sup> Profiles of the (002) diffraction line of the cokes heat-treated at  $1400$ — $1500^\circ\text{C}$  under 10 kbar were found to be composite, while no composite profiles were found with heat treatment of the same cokes under a reduced pressure of  $10^{-2}$  Torr.<sup>1)</sup> A kinetic study of the graphitization could not be carried out at a pressure as high as 10 kbar, because of the high rate of graphitization.

In the present work, the heat treatment of polyvinylchloride coke under pressures of 1, 3,

and 5 kbar was carried out for various durations at various temperatures, in order to learn the effect of pressure on the graphitization of carbon, and also to obtain more precise information on the composite profile of (002) diffraction.

### Experimental

**Sample and Apparatus.** The sample used was a graphitizing coke PV-7, which was also used in previous work.<sup>1)</sup> The coke was prepared by carbonizing polyvinylchloride at  $680^\circ\text{C}$ , and was examined spectroscopically and found to contain only negligible amounts of inorganic impurities. The coke had a particle size in the range of 0.1 to 0.4 mm.

The high pressure apparatus used was of a simple piston-cylinder type. It was made of tool steel, having a hardness of R. C. 64, and a bore diameter of 24 mm.

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1) T. Noda and H. Kato, *Carbon*, **3**, 289 (1965).

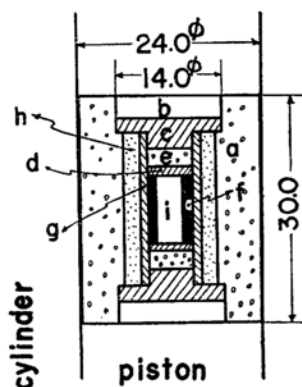


Fig. 1. Arrangement of the specimen cell.

a : pyrophyllite holder, b : metal disk (14 $\phi$ -3 mm), c : graphite terminal plate (14 $\phi$ -2mm), d : graphite plate (6 $\phi$ -1mm), e : pyrophyllite disk (6 $\phi$ -2.5mm), f : glassy carbon tube (6 $\phi$ -4 $\phi$ -10mm), g : graphite heater (8 $\phi$ -6 $\phi$ -21mm), h : boron nitride, i : sample

Such a piston-cylinder type apparatus made of tool steel has been known to last up to 10 kbar at room temperature.<sup>2)</sup> The whole apparatus was immersed in water for cooling during the experiment. The arrangement of the specimen cell is shown in Fig. 1. Boron nitride (h in the figure) was placed between a graphite heater and pyrophyllite in order to prevent chemical reaction between them. A glassy carbon tube (f in the figure) played the role of preventing contamination of the sample. A heating current was passed through the pistons into a graphite tube heater. The pistons were insulated from the cylinder by a composite sheet of asbestos and Mylar film. The temperature of the central part of the sample was evaluated from the relation between heating input power and temperature, which had been determined beforehand up to about 1200°C using a chromel-alumel thermocouple. The relations between input power and temperature were determined at different pressures and are shown in Fig. 2. A thermocouple inserted in the specimen probably makes a heat sink which may cause a small decrease in the temperature of the specimen. In most of the actual runs, no thermocouple was inserted in the specimen, and therefore the heat treatment temperature of the specimen could be a little higher than the temperature estimated from the input power. However, the difference may be within the error of temperature measurement, because the input power for the melting of platinum under 5 kbar (1800°C<sup>3)</sup>) with in same arrangement was exactly on the extrapolated straight line of the upper part of the curve for 5 kbar.

There was a very large temperature gradient in the specimen along the axial direction of the graphite heater, the temperature of the end part of the specimen being about 10% lower than that of the central part. The temperature of the specimen was controlled manually by regulating the input power. The error in

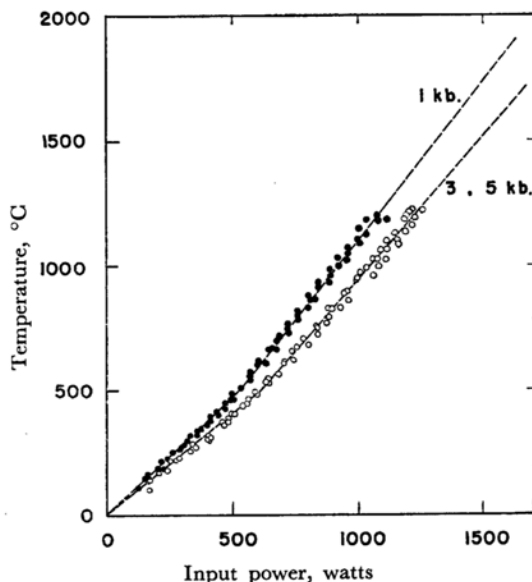


Fig. 2. Relations between input power and temperature under different pressures.

the determination of the heat treatment temperature was estimated to be  $\pm 50^\circ\text{C}$  at 2000°C from the scattering of the points in the relation between input power and temperature, and from the variation of input power regulation. The heating rate was about 1000°C/min and the specimen was cooled down to room temperature within a few minutes by cutting off the power. The maximum temperature which was attainable depended strongly on the arrangement of the specimen cell. By using the arrangement shown in Fig. 1, a temperature up to 1800°C was attained under 1 kbar, and 2000°C under 5 kbar.

The pressure was transmitted through pyrophyllite, so that quasi-hydrostatic pressure was applied to the sample. The pressure was calibrated by use of the phase transition of neutral ammonium fluoride, which occurs at 3.7 kbar with a volume change of about 28%.<sup>4)</sup> The error in the pressure measurement was estimated to be  $\pm 0.2$  kbar from the scattering of four independently measured values of the phase transition.

The heat treatments of the sample were carried out at temperatures ranging from 1100°C to 1900°C for 3 to 90 min under 1, 3, and 5 kbar. The central part (about 1 mm thick) of the heat-treated specimen was used for the X-ray diffraction analysis, in order to avoid ambiguity caused by the temperature gradient along the specimen.

**Analysis of X-Ray Diffraction Profiles.** The profiles of the (002), and (004) diffraction lines for the heat-treated specimen were measured by using a recording X-ray diffractometer and Ni-filtered  $\text{CuK}\alpha$  radiation. Most of the profiles obtained were composite, as can be seen in Figs. 3b), and c). All the composite profiles appear to have two peaks at around  $26.0^\circ$  and  $26.5^\circ$  in  $2\theta$ . The occurrence of a composite profile indicates that there must be more than one independent range to produce coherent scattering of X-rays,

2) T. Noda, H. Kato, T. Takasu, A. Okura and M. Inagaki, *This Bulletin*, **39**, 829 (1966).

3) W. Paul, "Solid under Pressure," McGraw-Hill, New York (1963), p. 175.

4) R. Stevenson, *J. Chem. Phys.*, **34**, 346 (1963).

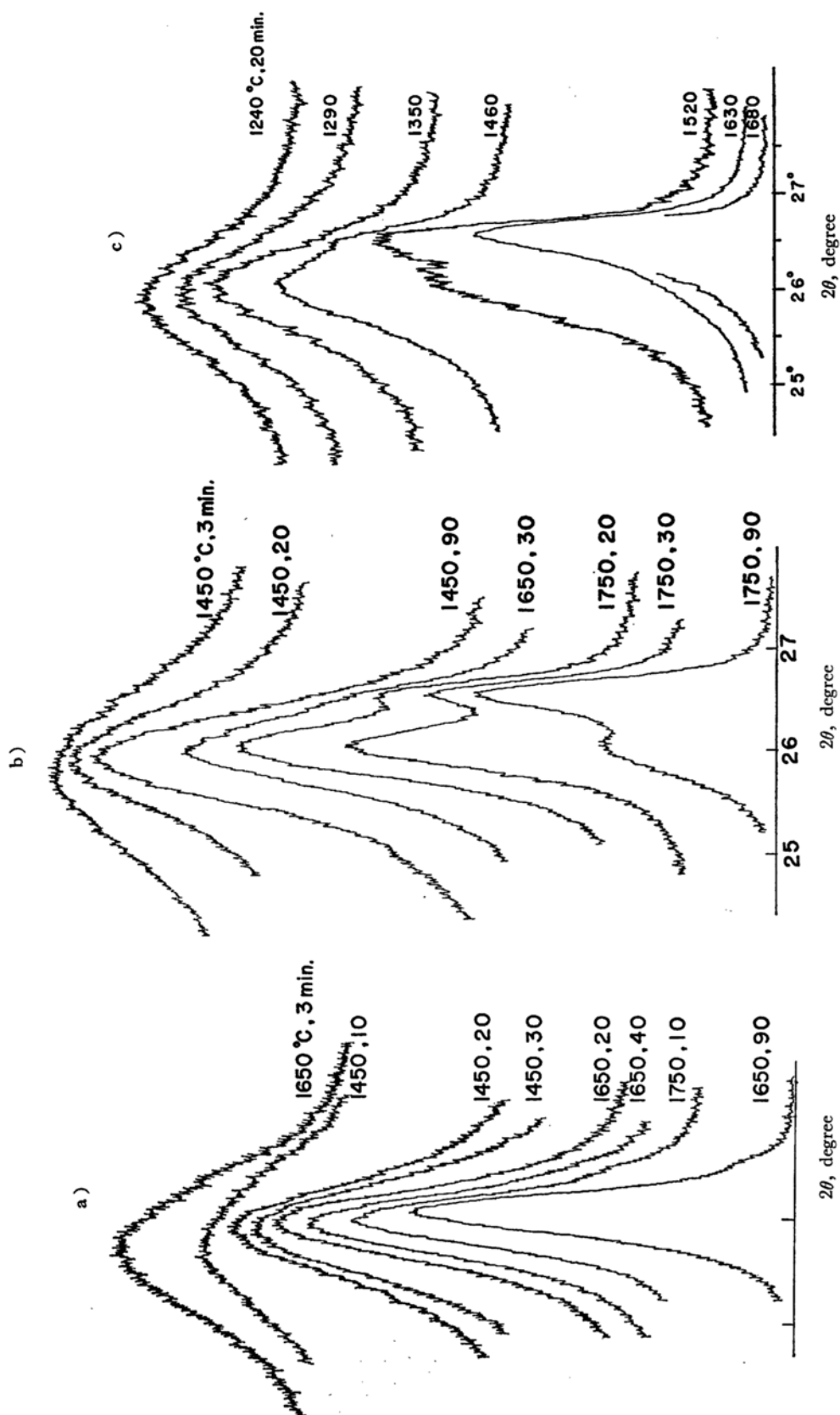


Fig. 3. Changes of the profile of (002) diffraction line a) under 1 kbar, b) under 3 kbar, c) under 5 kbar.

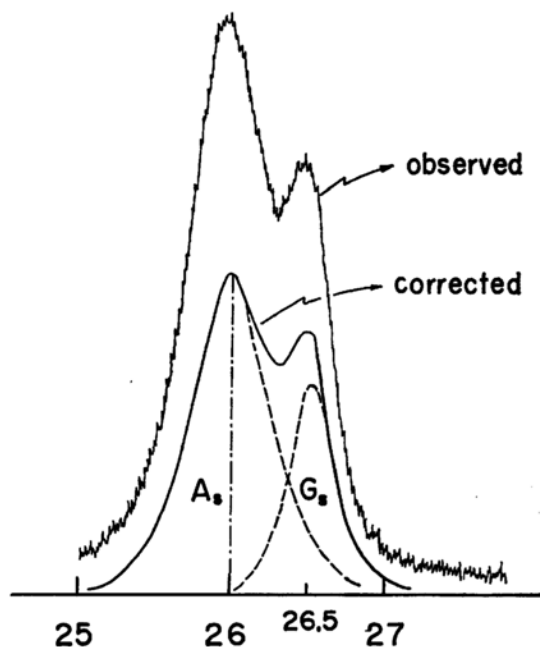


Fig. 4. Schema of separation of composite profile.

and therefore the composite profile can be separated into its component profiles.<sup>5)</sup> The procedure for the separation of an observed composite profile into its component profiles is illustrated in Fig. 4. After correction for the Lorentz-polarization, atomic scattering and absorption factors by the conventional method,<sup>6)</sup> the profile on the low angle side is folded at  $26.0^\circ$ , the reason for which will be described later. When the component profile at  $26.0^\circ$  is subtracted from the composite profile, the balance gives an almost symmetrical and sharp peak at around  $26.5^\circ$ . The components, correspond to the separated profiles at  $26.0^\circ$ , and at  $26.5^\circ$ , are designated as  $A_s$ , and  $G_s$ , respectively.\*<sup>2</sup> The areas under the separated component profiles were measured by using a planimeter, and the ratio of the area of the profile of the component  $G_s$  to the total area of the composite profile was calculated. This area ratio is sensitive to the preferred orientation of the crystallite in the specimen used for X-ray measurement. The correction of the area ratio for the preferred orientation was carried out by using the calibration curve, because the quantity of specimens for X-ray measurement was so small that direct measurement of the preferred orientation of crystallites in the specimen could not be carried out. The calibration curve was determined by using known mixtures of two kinds of petroleum cokes, one treated at  $1600^\circ\text{C}$ , and the other treated at  $3200^\circ\text{C}$ ,

5) T. Noda and M. Inagaki, "Proceedings of the Fifth Conference on Carbon Vol. I," Pergamon Press, London (1962), p. 559.

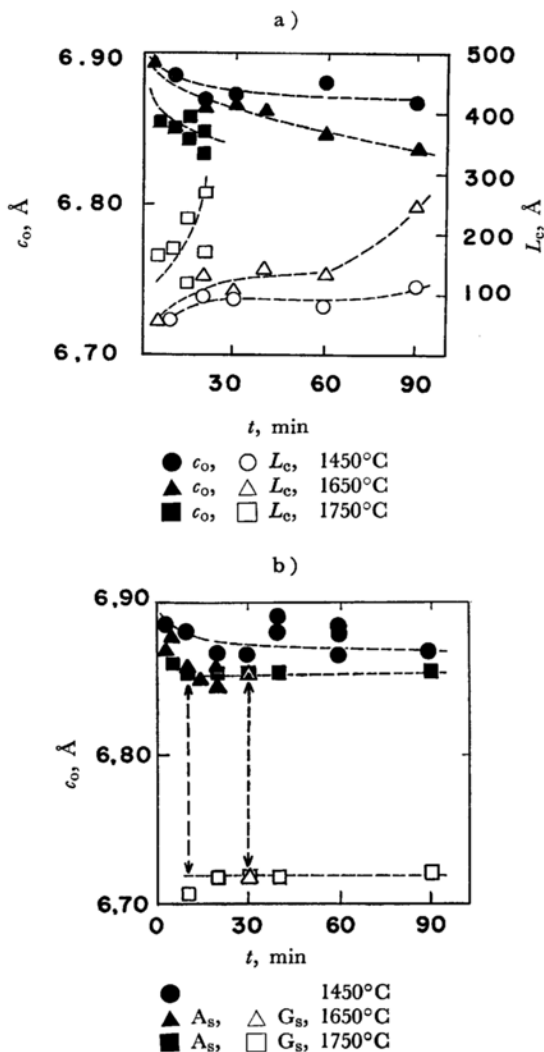
6) W. R. Ruston, *Fuel*, **32**, 53 (1953).

\*<sup>2</sup> For a hard carbon heat-treated under 5 kbar, the authors found a similar composite profile, which seemed to consist of two components. In the present work, the components of soft carbon were distinguished from those of hard carbon by using a suffix "s," because they might not have the same structures.

which have the same diffraction angles as those of the component profiles,  $26.0^\circ$ , and  $26.5^\circ$ , respectively.

## Results

Profiles of the (002) diffraction line for specimens heat-treated under 1 kbar are shown in Fig. 3 a). The diffraction angle of the line increased and its half-width decreased with increase in heat treatment temperature (HTT) and residence time, similar to the changes for heat treatments under room or reduced pressure. Changes of the (002) profile under 3 kbar are shown in Fig. 3 b). At low temperature and short residence time for heat treatment, the diffraction angle and half-width of the line changed the same as in the case of 1 kbar. When the diffraction angle of the line reached to

Fig. 5. Changes of  $c_0$ -spacing and crystallite size  $L_c$  with residence time.

a) under 1 kbar, b) under 3 kbar.

26.0°C, however, a new sharp peak for the component  $G_s$  appeared at 26.5°, overlapping the profile for the component  $A_s$ . With further heat treatment, this sharp profile for  $G_s$  developed without appreciable change in the diffraction angle. Almost the same changes in the profile of the (002) diffraction line were observed under 5 kbar (Fig. 3 c)), but the change occurred at lower temperature, or in a shorter time than in the case of 3 kbar. In the heat treatments under 3, and 5 kbar, the diffraction angle of the profile for the component  $A_s$  stayed unchanged at 26.0° after the appearance of the profile for the component  $G_s$ . This is the reason why the position of the profile for  $A_s$  was fixed at 26.0° when the observed composite profile was separated into its component profiles, as illustrated above.

Changes in the  $c_o$ -spacing and crystallite size  $L_c$  of the specimens heat-treated under 1 kbar with residence time are shown in Fig. 5 a). Comparing these changes with those of the same coke under reduced pressure,<sup>1)</sup> the accelerating effect of pressure on graphitization of carbon becomes very evident. In Fig. 5 b), the changes in the  $c_o$ -spacing of the specimens heat-treated under 3 kbar with residence time are shown. Under 3 kbar, the component  $G_s$  was observed to appear in 30 min at 1650°C, and in 10 min at 1750°C, while at 1450°C no indication of the component  $G_s$  was observed in 90 min. The crystallite size of the component  $A_s$  increased gradually from 100 to 200 Å, while that of the component  $G_s$  was about 300 Å. Change in the content of the component  $G_s$  with residence time is shown in Fig. 6. The content of  $G_s$  increased to about 50% in 90 min at 1750°C. Changes in the  $c_o$ -spacing of the components  $A_s$  and  $G_s$  of the specimens heat-

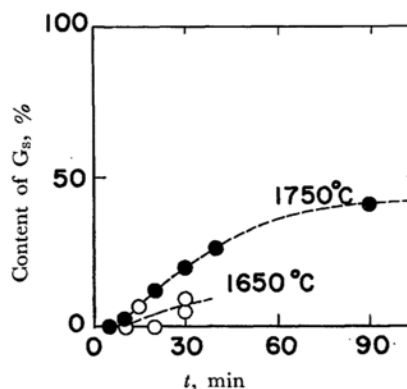


Fig. 6. Changes of content of the component  $G_s$  with residence time under 3 kbar.

treated under 5 kbar with HTT for various residence times are shown in Fig. 7 a). The  $c_o$ -spacing of the component  $A_s$  decreased to 6.85 Å around 1600°C in 3 min, around 1350°C in 20 min, and around 1300°C in 60 min. Changes in the content of the component  $G_s$  with HTT under 5 kbar are shown in Fig. 8 a). The intersection of these curves with the abscissa, or the temperature at which the component  $G_s$  begins to appear, should be about the same as those at which the  $c_o$ -spacing of the component  $A_s$  reaches 6.85 Å. The shape of the curves appears to be the same for different residence times, and they may be superimposed by translation along the abscissa. Such a superimposed curve for a residence time of 10 min is shown in Fig. 8 b). It is evident that the superimposition works quite well. Therefore, the curves for  $c_o$ -HTT and  $L_c$ -HTT were translated by the same amount. The superimposed curves make it easier

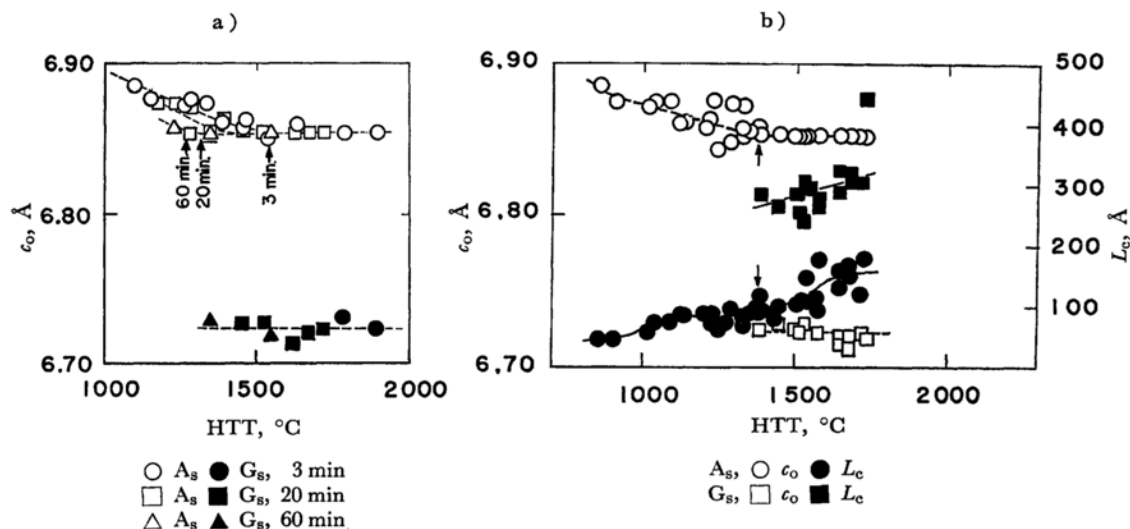


Fig. 7. Changes of  $c_o$ -spacing and crystallite size  $L_c$  with HTT under 5 kbar.

a) for different residence times, b) superimposed curve for the residence time of 10 min

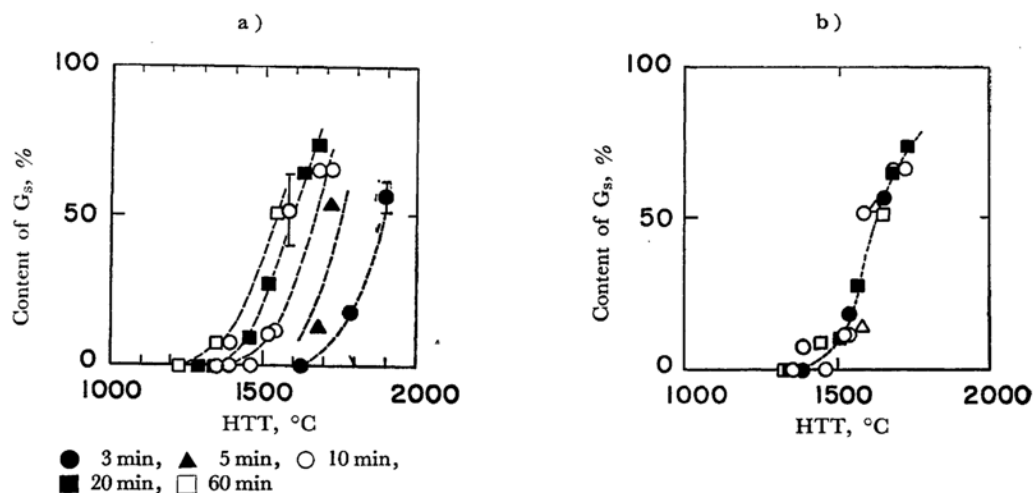


Fig. 8. Changes of content of the component  $G_s$  with HTT under 5 kbar.

a) for different residence times    b) superimposed curve for the residence time of 10 min

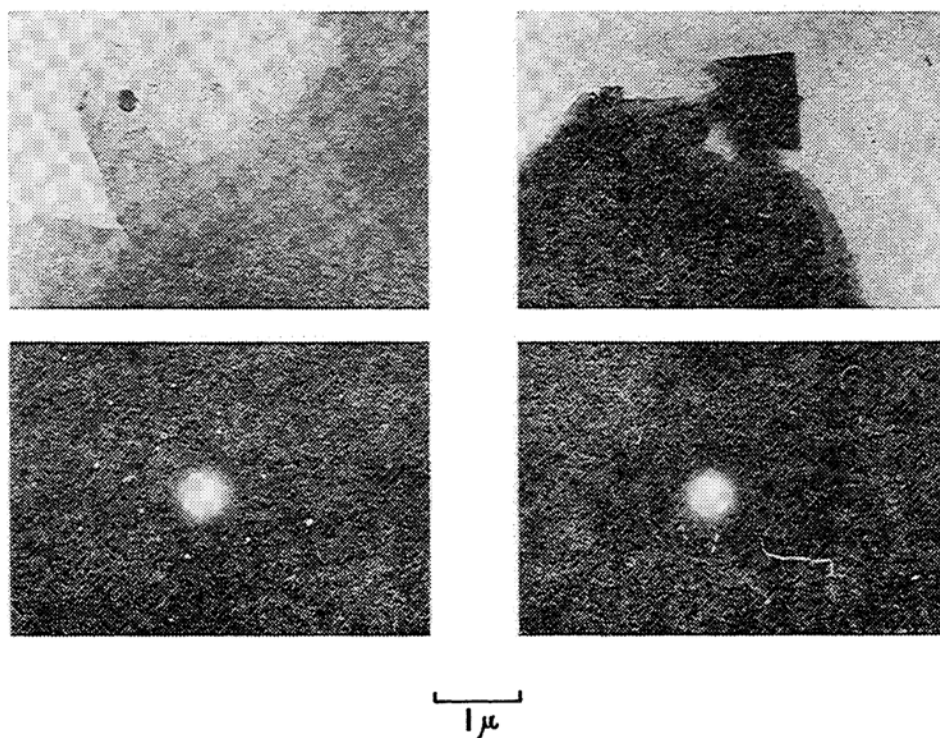


Fig. 9. Electron micrographs and electron diffraction patterns for the specimen heat-treated at 1720°C under 5 kbar.

to view the general trends of the changes in  $c_o$  and  $L_c$  with HTT (Fig. 7 b)).

From these figures, it can be seen that the graphitization of carbon under 3, and 5 kbar seems to proceed as follows. In the early stage of graphitization, there is one component  $A_s$ , of which the  $c_o$ -spacing decreases from the original value of

6.91 Å to 6.85 Å, and the crystallite size  $L_c$  increases to about 100 Å. In the next stage, the component  $G_s$  appears, and its content increases rapidly with increase in temperature and residence time for heat treatment. The  $c_o$ -spacing of the components  $A_s$ , and  $G_s$  remain unchanged at 6.85, and 6.72 Å, respectively. The crystallite sizes  $L_c$  of the

components  $A_s$  and  $G_s$  are about 150–200 Å, and 300 Å, respectively.

### Discussion

In a previous work,<sup>1)</sup> composite profiles were also obtained in cases where a rapid change in the  $c_o$ -spacing was observed. It was suggested that there might be a possibility that each specimen used for X-ray study was a mixture of carbons heat-treated at different temperatures because of the steep temperature gradient in the specimen. In the present work, pyrophyllite disks (e in Fig. 1) were inserted between the specimen chamber and the graphite terminal plates in order to minimize the temperature gradient in the specimen. Even in this modified arrangement a temperature difference was observed between the end and the central parts of the specimen, the temperature of the end part being about 10% lower than that of the central part, as mentioned previously. In addition to the temperature gradient, the pressure gradient along the specimen must be taken into account. The pressure at the end part of the specimen may be a little higher than that at the central part. The (002) profile of the end part of the specimen of which the central part had a composite profile was also composite, and its only difference from the central part was the degree of the development of the component  $G_s$ , the content of  $G_s$  for the end part being smaller than that for the central part. This seems to show that temperature and pressure gradients along the specimen were not the cause of the occurrence of a composite profile. The temperature difference itself affected the content of the component  $G_s$ . In other words, the structural change in the specimen under pressure was properly reflected in the diffraction profile.

In the graphitization process of PV-7 under a pressure of 3–5 kbar, there exist the components  $G_s$  and  $A_s$  side by side in the one specimen. In the early stage, there is only one component  $A_s$ , of which the mean  $c_o$ -spacing gradually decreases to 6.85 Å and the crystallite size  $L_c$  increases a little. In the next stage, in which the  $c_o$ -spacing of the component  $A_s$  has reached 6.85 Å, the component  $A_s$  begins to transform into the component  $G_s$ , and the main change at this stage is the increase in the content of the component  $G_s$ . The  $c_o$ -spacing of the component  $A_s$  stays unchanged at 6.85 Å, and its crystallite size  $L_c$  also remains unchanged at around 150–200 Å through this stage. The  $c_o$ -spacing of 6.85 Å is a little but evidently smaller than that of the so-called turbostratic structure, 6.88 Å. If the  $c_o$ -spacing of one component is assumed to be 6.88 Å, the balance of the profile becomes strongly un-symmetrical, and it is necessary to assume it consists of more than two components. The  $c_o$ -spacing of the component

$G_s$  is 6.72 Å and its crystallite size  $L_c$  is around 300 Å. The spacing of the component  $G_s$  measured from the (004) diffraction line is also 6.72 Å, and is clearly not 6.71 Å. Even though this spacing of 6.72 Å is a little larger than the spacing of natural graphite, 6.708 Å, specimens having a high content of the component  $G_s$  were found by X-ray diffraction to have a three dimensional structure, and by electron microscope and microdiffraction to contain flaky particles of which diffraction pattern was of the perfect six-fold symmetry of single crystal (Fig. 9a)). In the same specimen, however, some other particles showed continuous diffraction rings (Fig. 9b)). It is known that the  $c_o$ -spacing of the cokes graphitized as highly as possible can hardly be reduced to that of natural graphite.<sup>7)</sup>

Phenomenally, the change in profile in the second stage of graphitization under a pressure of 3–5 kbar is similar to the so-called two-, or three-phase graphitization of non-graphitizing or hard carbons. The occurrence of a composite profile,

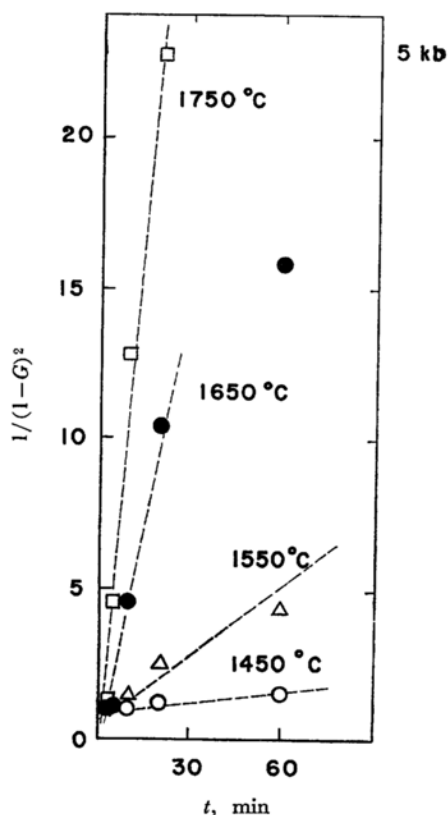


Fig. 10. Relations between content  $G$  of the component  $G_s$  and residence time  $t$ .

7) T. Noda and M. Inagaki, This Bulletin, **37**, 1709 (1964); T. Noda and H. Matsuoka, *Kogyo Kagaku Zasshi (J. Chem. Soc. Japan, Ind. Chem. Sect.)*, **63**, 465 (1960); P. L. Walker and G. Imperial, *Nature*, **180**, 1184 (1957).

which was composed of the components  $G_s$  and  $A_s$ , indicates that ranges having graphitic and non-graphitic structures have a sufficient extent to produce independent coherent scattering of X-ray in one specimen.

Under 1 kbar, no composite profile was observed and the  $c_o$ -spacing decreased continuously to 6.78 Å without the appearance of the second peak for the component  $G_s$ . This means that not a sufficient extent of lattice, having graphitic structure to produce coherent X-ray scattering, was formed in the specimen by the treatment, so that only a homogeneous decrease of the  $c_o$ -spacing was observed.

From these experimental results, it can be concluded that the accelerating effect of pressure on the graphitization of carbon increases with pressure. However, the graphitization process above 3 kbar seems to be different from that below 3 kbar.

For experiments under 3, and 5 kbar, an approximate relation between the content,  $G$ , of the component  $G_s$ , and residence time  $t$  was investigated, although the accuracy of the measurements of temperature and pressure of heat treatment were not good enough, and also experimental data was not abundant enough for a quantitative kinetic analysis of graphitization under pressure. A relatively good linearity between  $1/(1-G)^2$  and  $t$  was obtained (Fig. 10). By using the experimental rate constant, the activation energy was calculated to be 80–120 kcal/mol, and the activation volume –7––9 cc/mol at temperature of 1650–1750°C.

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